Details of a few simple changes in the Musician’s Amplifier to improve performance and listening quality.

Inc r e as i ng P o w e r O u t p u t

Recently there appeared in the literature an article which described a power amplifier circuit which is between a tetrode and triode in characteristics and performance. This circuit requires an output transformer which is understood to have a tap at 43 per cent of the turns from center to each plate. Although not shown on the circuit diagram, the output transformer specified in the original Musician’s Amplifier article has a center tap in each half of the primary winding, which is at 50 per cent of the winding, not too far from 43 per cent. As the circuit has certain features of interest, we investigated the possibility of using the taps to adapt the Musician’s Amplifier and improve its performance. An amplifier was built with an A-B switch, arranged so that in one position the circuit was the conventional Musician’s while in the other position the screens were connected to the center taps of each half primary. The results were checked on an intermodulation analyzer and proved to be encouraging. At low powers, say up to 7 watts, there is no difference in distortion, both being under 1 per cent IM and most of the way both are way under 0.5 per cent. Above 7 watts, the Musician’s Amplifier begins to have increasing amounts of IM reaching 8 per cent at 12 watts. At this power the tapped connection amplifier is still under 1 per cent, and its IM distortion does not begin to climb until the power output is 16 watts, reaching 8 per cent at 19 watts. These results are summarized in Figs. 2 and 3. It must be emphasized that the above power figures are those as read on the 1M meter and are not equivalent sine-wave power. If the figures are converted to equivalent sine-wave power by multiplying by the factor 1.47, then the power output at 8 per cent is 27.9 watts, while the equivalent sine wave power at 1.5 per cent IM is 22 watts. Effectively, the power output has been increased to 158 per cent of its previous value. This is certainly a worthwhile improvement—particularly when it costs no more than two pieces of wire and eliminates the two 100-ohm resistors which tie the screens to the plates.

Operation

Checks were made on the effect of the change on the plate and screen currents and on dissipation at both full-signal and quiescent conditions. It was found that the tubes were operating within safety ratings so that satisfactory tube life may be expected. Checks also were made on the response, square-wave performance, and source impedance; these were found to be affected very little. One item of importance was found: as originally described, the circuit is very nearly Class A and the power amplifier is operated toward the upper regions of plate dissipation ratings, but well within ratings. The bias on the final stage was increased so as to go toward Class AB operation. It was found that any move toward higher bias caused the IM distortion to climb, even at relatively low power levels. The original bias resistor of 250 ohms gives optimum results with the new connection.

By going to the tapped connection for the screens, the gain of the amplifier without feedback is increased by about 4 db. With a 4700-ohm resistor supplying feedback voltage from the 16-ohm output connection, the gain increase by using the taps is around 0.5 db or less. Thus the amount of feedback is increased to around 24 db. With most of the amplifiers converted by the authors, there is no tendency toward instability either at sub-audible or supersonic frequencies. Depending on the capacitance and condition of decoupling capacitors, it is possible that a tendency of the loudspeaker to “breathe” or oscillate slowly at 1 cps or less may be encountered. It is recommended that when the change to tapped operation is made, the feedback resistor be increased to 6800 ohms. This value will provide 20 db of feedback, and tests have shown that no appreciable increase in distortion results. For other secondary connections, the feedback resistor may be figured as 1700 times the square root of the nominal secondary impedance.

One of the most interesting and important features of the Musician’s Amplifier is the way in which it overloads. Sine-wave power output tests can be made conveniently, quickly, and more accurately than might be supposed, by feeding in a sine-wave signal and increasing the input level until the waveform of the output as seen on a cathode ray oscilloscope begins to clip at the tops and bottoms, or begins to get “bumps” on the sides at low frequencies. The original amplifier overloads so...
smoothly that it is often difficult to tell just when the beginning of overload is reached. Furthermore, when the tops and bottoms of the waves are being clipped, after overload really is evident there is no ringing or fuzz, but only a clean clip. With the change to the screen tap connection, it was found that the overload was just as smooth as with the conventional triode connection.

Some inquiries have been made as to whether or not a large capacitor should be connected across the self-bias resistor of the output stage. It is well known that a large bypass capacitor should be connected across the bias resistor in Class AB stages, as this improves operation at the higher power levels. During the original work, the bypass capacitor was tried and was abandoned because it produced no significant effect. This is because the power amplifier is practically pure Class A. With the tapped arrangement the capacitor was found to have an improving effect at higher power outputs. For maximum power output connect a 50-µf 50-volt capacitor across the bias resistor. However, it can be omitted with the assurance that no noticeable difference will be heard at lower levels.

Listening Tests

Of course the final test of the merits of an audio circuit is now and probably ever shall be the listening test. In music, listening quality is everything. Having an amplifier with an AB switch is an advantage in listening tests, and after considerable listening it is our opinion that the change does improve the sound, particularly on fortissimo musical passages when played at concert hall level. At the usual apartment house living room loudness, operation of the switch produces very little noticeable change. Several users tell us that after living with modified Musician’s Amplifiers for several weeks, they are convinced that they sound better at all loudness levels. For those who have built the Musician’s Amplifier as originally written up, with the specified output transformer, here are the details for making the conversion:

1. Remove both 100-ohm resistors \(R_{e2}\) and \(R_{e3}\) on the schematic that tie screens to plates of the output tubes.
2. Connect a wire from the screen of the tube whose plate connects to terminal 1 of the transformer to the adjacent terminal 2.
3. Connect a wire from the screen of the other output tube (its plate connects to terminal 6 of the transformer) to terminal 5.
4. Change the feedback resistor from 4700 ohms to 6800 ohms (or to a value equal to \(1700/\sqrt{2}\) if an output impedance other than 16 ohms is being used).

Output Tubes

In the original paper, the authors used the 807 as an output tube in place of the inserted words “oil-filled capacitors” in the text material. The accompanying photograph showed round cans in the power supply, and the authors had much correspondence as to where round can oil-filled 8-µf electrolytic capacitors could be obtained. The answer is simple: the photograph was made with 8-µf electrolytic capacitors. In a number of cases when they could be obtained at reasonable prices, oil-filled capacitors have been used; however, the cans have not always been round. Oil capacitors of 6 or 8-µf, will give a hum-free amplifier. The voltage rating should be at least 600 volts.

The original power supply showed two filter chokes and three filter capacitors. We have found that there is no hum in an amplifier powered from a supply containing only one choke and having two filter capacitors of 6 or 8-µf. The reason for the use of only one choke is

![Fig. 2. Intermodulation distortion curves for the original Musician’s amplifier (dotted line) and for the converted model (solid line).](image1)

![Fig. 3. Power output vs. frequency curves for original and converted amplifiers.](image2)

KT-66 valve used in Williamson’s design. At that time the KT-66 was not available in America, although it is now.

Recently Tung-Sol Electric, Inc. introduced the 5881 tube which is, in effect, a single-ended 807. The total plate and screen dissipation in the triode connection is 26 watts with a plate-to-cathode voltage of 400. It has the further advantage of single-end construction and the now almost standard octal base. The 5881 has been used in the Musician’s Amplifier, both in the original model and in those converted to Ultra-Linear operation, and has been found to be very satisfactory from all angles—performance, tube life, cost, and appearance. These tubes are manufactured to a high degree of uniformity, so it is no longer necessary to purchase them in matched pairs. The ruggedized construction minimizes changes in element spacing and the consequent changes in characteristics—with heating or mechanical vibration. Because of these advantages, the 5881 is now our standard output tube.

Power Supply

There have been several changes in the power supply which warrant a discussion. In the original paper, the editor to cut down on the d.c. voltage drop in the power supply filter.

Another change in the power supply is in the rectifier tube. The original paper recommended a type 5V4G rectifier. The 5V4G or the older 83V were considered, and their advantage in having a lower internal tube voltage drop was fully recognized, but they were not used because of some past experience with internal tube leakage or shorts. The 5V4G tubes have become readily available because of their wide use in TV receivers as dampers, and it appears that modern construction has made them quite reliable. Thus, we now recommend that the 5V4G be used as a rectifier for improved results. The voltage surge during warmup is practically eliminated with this tube.

With these changes, the output voltage under full load is around 440 volts measured from B plus to ground. With a cathode bias on the output stage of 40 volts, the d.c. plate voltage as measured from plate to cathode on the 5881 tubes is just about 400 volts. With these voltages on the tubes, the cathode current

[Continued on page 30]
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**GILDING THE LILY**

[from page 14]

is around 63 ma, and no trouble should be encountered in obtaining the power levels or the low distortion of the Musician's Amplifier. Hum and noise in the power amplifier are inaudible.

**Front End**

The authors are well aware of the fact that no "front end" or preamplifier was described in the original paper and have had much correspondence with readers on the subject. Subsequent to the original paper, articles on front ends have appeared in these pages as well as in other publications. Some have been complex and expensive; others have been simple and inexpensive. In our own case, of course we have built front ends; some of these have been good, while others have been not so good. One of the big reasons for our not describing a front end has been that we have not been so sure of the features to be incorporated in the ideal front end and the almost unsurmountable obstacle to the amateur constructor in achieving the appearance of a factory built unit.

The requirements for a front end for the Musician's Amplifier are many and most rigorous: (1) It must have very low distortion; (2) it must have very low noise and hum level; (3) if must have a response which approaches, at least, that of the power amplifier; (4) it must be capable of being installed at some distance from the power amplifier with absolutely no degradation of performance; (5) it must provide a high-quality preamplifier for magnetic phonograph pickup; (6) it must provide adjust-
ment to compensate for the various recording equalization curves in use today or which have been widely used in the past; (7) it must have facilities for "tone compensation or adjustment" in addition to phono compensation, and which do not degrade the quality of program material or sound; (8) it must have medium-gain, flat-response inputs for FM tuner and tape; (9) it must have (for the benefit of the ladies) eye appeal and particularly must have a minimum of knobs and adjustments; (10) and perhaps most important, it must be moderate in cost without degradation of performance or facilities. This is a big order, and while we have built front ends which meet most of the electrical requirements, they often did not look good enough to warrant an article, largely because of our lack of manufacturing facilities.

We have now adopted the Altec Lansing A-433A remote amplifier as a very satisfactory front end. It meets all of the requirements laid down above and when the price is considered it is far less expensive and eminently more satisfactory for the amateur to buy than to attempt to duplicate with the usual home facilities. Furthermore, the connection of the A-433A to the Musician's Amplifier is very simple and can easily be done by anyone reasonably handy with a soldering iron and a few tools. The output of this front end is a cathode follower with output impedance of less than 1000 ohms so that no high frequencies are lost in cable capacitances.

When this front end is used, the combination should be perfectly stable. If motorboating is encountered, check filter capacitors in power amplifier. If at a maximum bass boost the speaker cone "breathes" subaudibly, decrease the value of the coupling capacitor between front end and power amplifier to 0.03 μf or decrease grid resistor from 1.0 meg to 0.47 meg. No audible difference in sound will be apparent.

The A-433A when used in conjunction with the Musician's Amplifier has more than adequate gain, particularly on phono input. At settings of the volume control which give very loud volume with low-output pick-ups there should be no audible hum. At full rotation of the volume control some hum may be heard, but not all of this comes from the front end. Some will come from stray magnetic fields, poor shielding on pick-up leads, etc. The hum level may be adjusted for optimum by removing the ground from heater center tap and connecting a ground to the moving arm of a 50-ohm pot across the heaters. With this arrangement, we have been able to reduce to almost inaudible levels the hum heard when on phono, the volume control wide open (far more than ever needed) and nothing connected to the input.

The authors wish to acknowledge the invaluable assistance of Ralph Ellison in constructing the experimental models of the amplifier.

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Write for characteristics and performance data

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LETTERS

Un-gilding the Lily

Sir:

In your July issue you make use of the expression "Gilding the Lily." I hope you will not take it amiss if I point out that this is actually a misquotation. I think the original observation about improving the lily was made by Shakespeare, in King John, Act IV, Scene 2, in the following words:

"To gild refined gold, to paint the lily,
To throw a pearl on the电压."

I am not suggesting that because Shakespeare said something in the 16th century we must forever use the same thing; but I do think that a perusal of these lines shows that the expression "To paint the lily" has some meaning, whereas to talk about "gilding the lily" has none.

C. A. Briggs,
Wharfside Wireless Works,
Idle, Bradford,
Yorkshire, England.

*(Italic ours—An un-gilded lily to Mr. Briggs for his comment. Since the misquotation is better known than the quotation, we followed popular belief. Ed.)

Sir:

We note with interest the article "Gilding the Lily" by Sarser and Sprinkle in the July issue of AE. Since the important portion of the article deals with the Ultra-Linear conversion, a circuit arrangement which we have designed, we feel privileged to comment.

The authors mention that the original Ultra-Linear circuit has a tap at approximately 43 per cent of the primary winding, and that they use a tap at 50 per cent which is "not too far from 43 per cent." What they fail to mention is that in our own circuit arrangement the screen feed is 1220 ohms, and in their arrangement it is 2500 ohms. We know that 2500 ohms is too far from 1220 to give comparable results and that the performance of the circuit is degraded through misuse, although there is measurable improvement in their arrangement over the conventional triode connection.

Our patent claims cover the use of any primary tap in this circuit arrangement. However, we have restricted the use of the term Ultra Linear to the condition where the dynamic plate characteristic curves are most linear. This occurs with tubes of the 6L6 and the 807 type with a primary impedance of 6000 ohms, screen impedance of 1200 ohms, and a load equal to 10 per cent of the plate-to-cathode voltage. Only this last condition has been met by Sarser and Sprinkle and it is therefore incorrect to refer to the Gilded Lily as Ultra-Linear.

David Haller & Herbert I. Keros,
Acro Products Company,
369 Shars Lane,

Phase Inverter or Phase Splitter?

Sir:

While explaining the audio circuit to an electrical power engi neer recently, I pointed out what I called a "phase-inverter" circuit. He examined the diagram carefully and woke me up to a long existing semantic difficulty by asking, "But isn't any amplifier stage a phase inverter?"

Without going into the question of certain circuits which do not invert phase, I had to say yes, and proceed to point out that "phase splitter" might be a better term. With that in mind, he looked at the diagram again and in a few seconds understood it completely.

So there it is, staring us in the face. Electronics, being a branch of a major science (physics), is supposed to encourage a certain amount of precision of expression among its practitioners, at least when a precise term is no more complicated and takes no longer to say than a loose one. Never again, in any of my writings, will I willingly be guilty of mentioning a phase inverter when I really mean a phase splitter. If someone comes along with a better term, I will use that. Do I hear a chorus of "me, too's"? I hope so.

While we are on the subject of terminology, how about adding the word "electronics" officially to the electronic lexicon? A conglomeration of wheels, levers, brackets, and other parts which constitute a unit that does some kind of a job as a whole is termed a mechanism. But its electronic counterpart defies

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