

1. Summary

Steanes Model 976B & Speaker Combo. Serial No. 2466.

12AX7 microphone gain stage with volume pot to 12AX7 mixer stage, with PU input through volume pot to mixer stage. Output of mixer stage to tone control and then to 12AX7 feedback input stage to cathodyne phase splitter. 6M5 push-pull output stage with common cathode bias. Output transformer secondary with separate feedback winding, and floating 100V distribution. 6V4 full-wave rectifier with two RC droppers.

Excellent condition. Original white plastic Steanes badge on top grill, but 1958-9 manufacture date indicates Philips manufacture with Steanes badging. Green thread lock marked fixings.

Components

Power Transformer '344.096', '4x9'. 250-CT-250, 6V3 ~3A, 6V3 ?A.

Output Transformer 'TYPE 903'. 0219 with VSNP stamp. 8k2Ω PP (DCR=190Ω); 0-250Ω-500Ω-1000Ω (50-70-100V); 1.5Ω F-FB.

CAPs Ducon 24uF 300V 28 48 38

Ducon ET1B 58 68 58

Ducon High Seal 118

Pots IRC 86 or 8G curve C

Tubes (all Miniwatt) 6V4 Miniwatt 8K kC 8J (kC=6X4, 8=1958 or 68)

6M5 Miniwatt 9A M+ 8L (M+=EL80=6M5; 8=1958)

6M5 Miniwatt 8H M+ 8G (M+=EL80=6M5; 8G=1958 ??)

12AX7 Miniwatt 8I mC6 Δ8G (Philips Herlin 1958)

12AX7 Miniwatt 8K mC6 Δ8I (Philips Herlin 1958)

Two open-backed speaker boxes that join back-to-back with clips, such that amplifier and cables fit inside to provide a single unit with one carry handle. Dark green vinyl with red piping on plywood. Each box with Rola M 8" speaker (7W, 2Ω coil, F57 cone) and Rola (CEL58 8M36B) isocore potted speaker transformer (date stamp 21 Mar 1956) with 2k5Ω:2Ω ratio, with parallel wiring to amplifier (1250Ω loading). Vinyl and speaker cloth in very good condition. A few minor hairline tears near rim of cones.

Issues:

No power switch. Old wax and electrolytic capacitors. Mains wiring close to circuitry. Floating speakers. Spare 6V3 winding. Not the best grounding. Speakers use line transformers.



1.1 Modifications for Guitar Amplifier

- Main fuse changed to 0.5A slow blow.
- Fuse added to PT secondary CT (0.2A Fast IEC127 5x20).
- 1N4007 added in series with each rectifier plate for 6V4.
- Improved grounding scheme.
- On switch added to rear panel.
- Electrolytics and wax coupling caps replaced.
- PU Volume pot replaced with dual gang and used as post-PI volume.
- Grid stoppers added.
- 6M5 cathode 1Ω sense resistors added.
- 6M5 screen stoppers increased, and extra screen supply filtering.

- 2x 330VDC 90pF MOVs added across each OT half-winding. RC network removed from across PP.
- OT secondary grounded.
- Neoprene feet pads.
- Replace 12AX7 stages with 12AU7 to reduce gain.
- Added 1.6H choke to VS2 supply.
- Re-biased input stages for better use of 12AU7.

To do:

- Replace rubber feet.
- Methyl cellulose based glue, and thin Kozo paper for speaker cone repair.
- Suspect V3 valve socket – heater sometimes doesn't connect – confirm both 6M5 heaters are on!

2. Measurements

Voltage rail regulation. Modified circuit.

Rail	240VAC mains VDC, VACrms Idle condition (12AX7, no choke)	240VAC mains VDC, VACrms Idle condition (12AU7 changes)
VS1	300, 5.1 (340V turn-on pk)	300, 5.4 (340V turn-on pk)
VS2	288, 1.6	280, 0.3
VS3	250,	250,
VS4	235,	225,
Cathode	9.8 (27+27mA) 7.5W	9.8 (27+27mA) 7.5W
Heater 1	6.6	6.6
Heater 2	?	?
Sec HT	264-0-264	264-0-264
V1A,B	132V, 132V, 1.3V	102V, 108V, 4.8V
V2A	120V, 1.03V	139V, 2.5V
V2B	60, 192 1.35V	88, 168 1.35V

Power transformer primary DC resistance: 30Ω (BLU-BLK); 26Ω (RD-BLK).

Power transformer secondary DC resistance: 185+185Ω.

Heater current requirement is: $2x 0.71 + 2x 0.3 + 0.6$ (6V4) = 2.6A indicates a 260-CT-260, 6V3 3A, 6V3 ~0.5A.

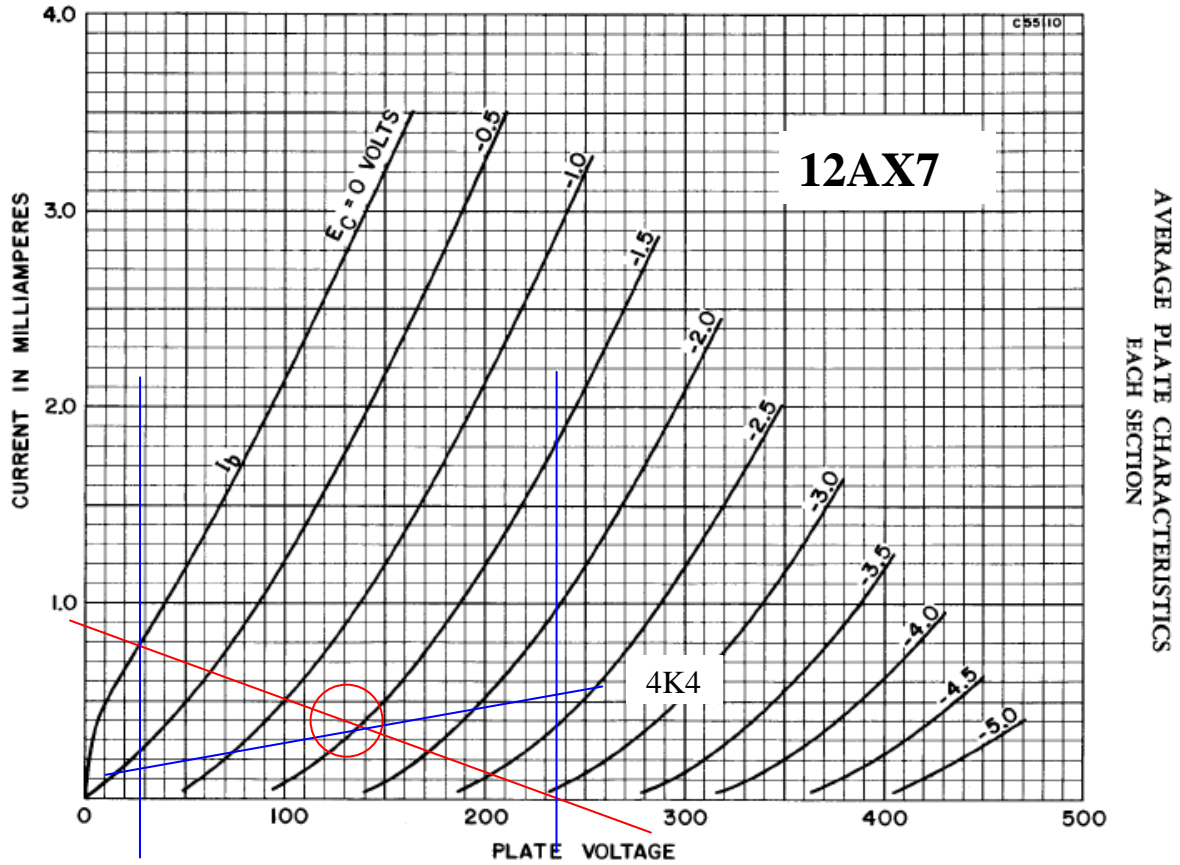
OT with 1.1kΩ resistive load:

Cranked output up to 108VAC (10.6W). Hum negligible. Hiss noticeable but minor.

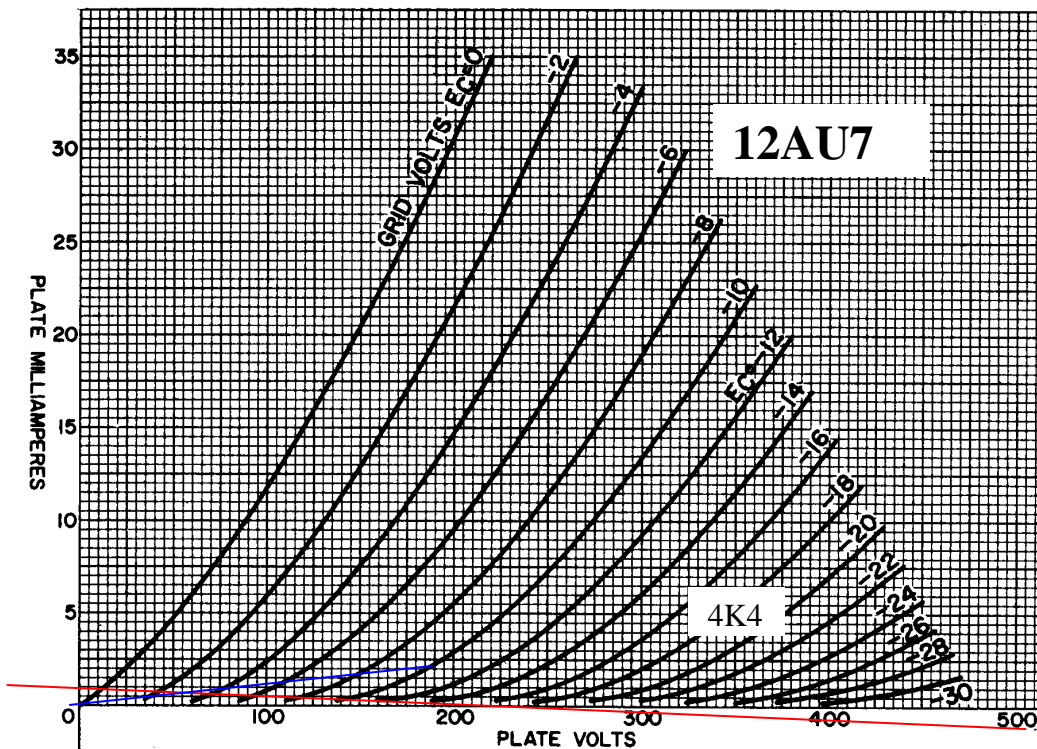
3. Design Info

3.1 Input stages 12AX7

For the first two 12AX7 stages have a common $2k2\Omega$ cathode bias; V1A-V1B; VS4 = 235V; Va=132; Rk=4k4; Vk=1.3V; Ia=0.37mA; RLdc=270k Ω .

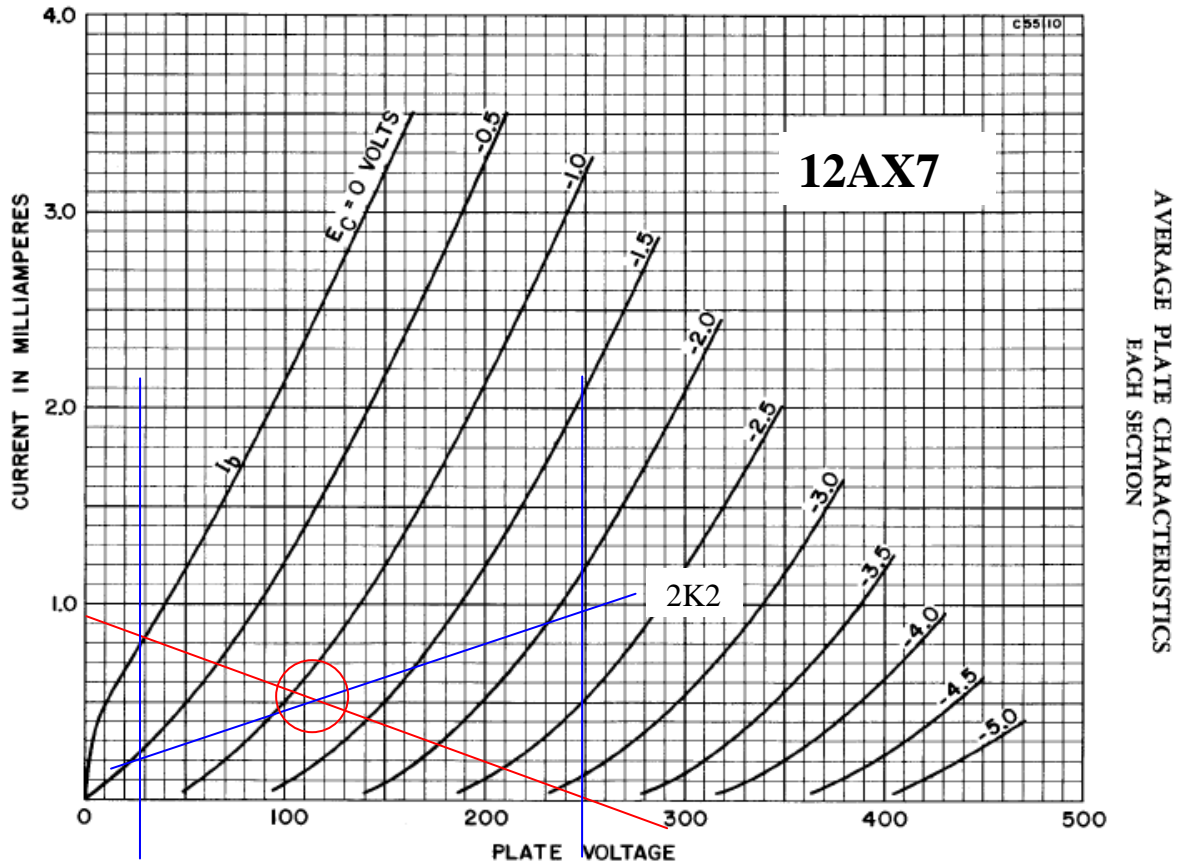


Changing to a 12AU7 will draw more current, and raise the cathode bias to ? The anode load should be reduced from 270k to about 100k, and the supply dropper reduced from 27k to 15k.

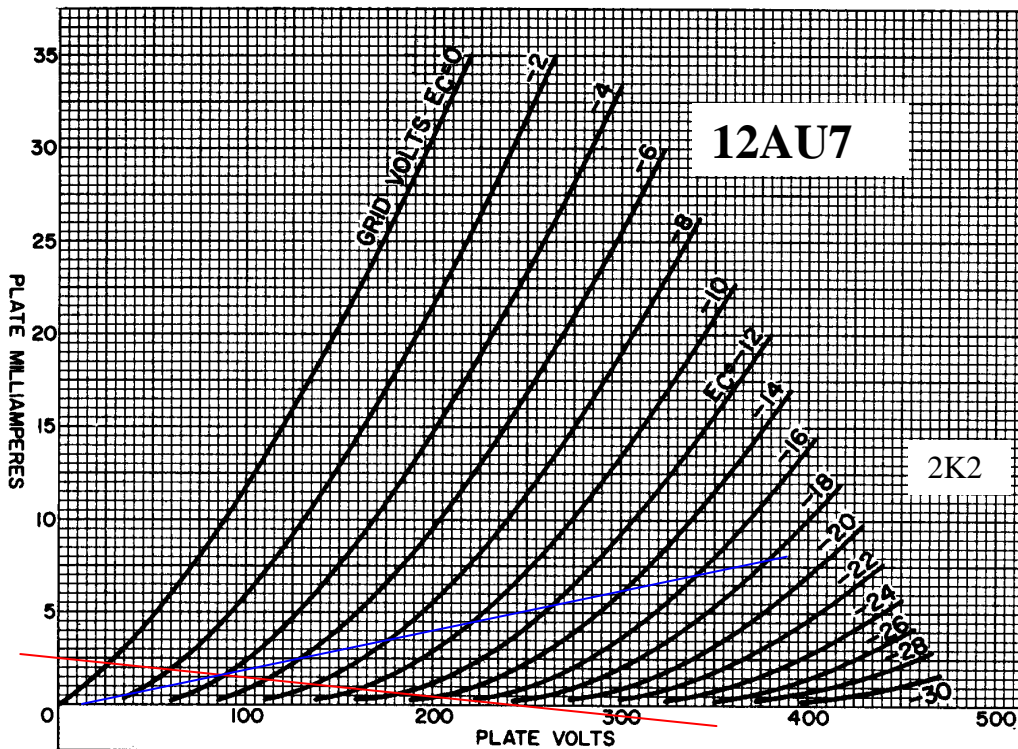


3.2 Feedback stage 12AX7

The feedback 12AX7 stage; V_{2A} ; $V_{S3} = 250V$; $V_a=132$; $R_k=2k2$; $V_k=1.03V$; $I_a=0.37mA$; $R_{Ldc}=270k\Omega$.

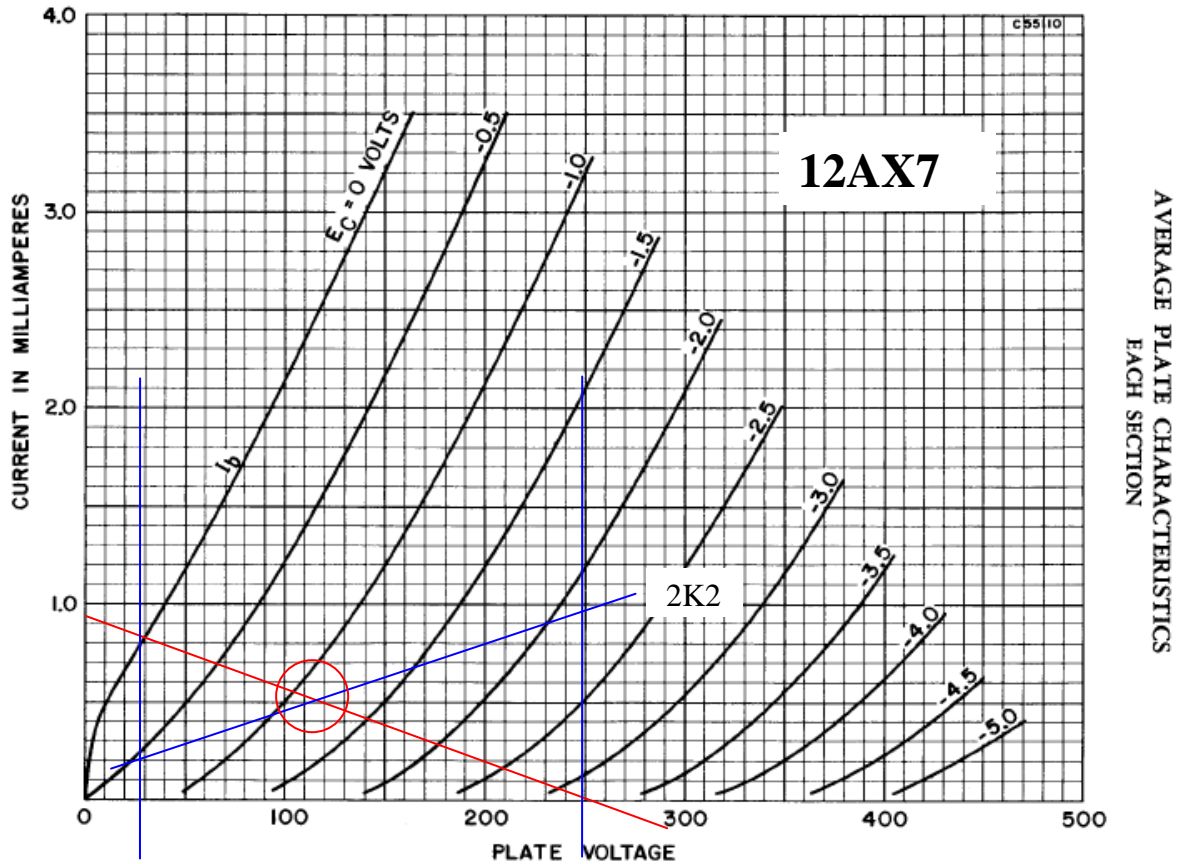


Changing to a 12AU7 will draw more current, and raise the cathode bias to ? The anode load should be reduced from 270k to about 100k, and the supply dropper reduced from 27k to 15k.

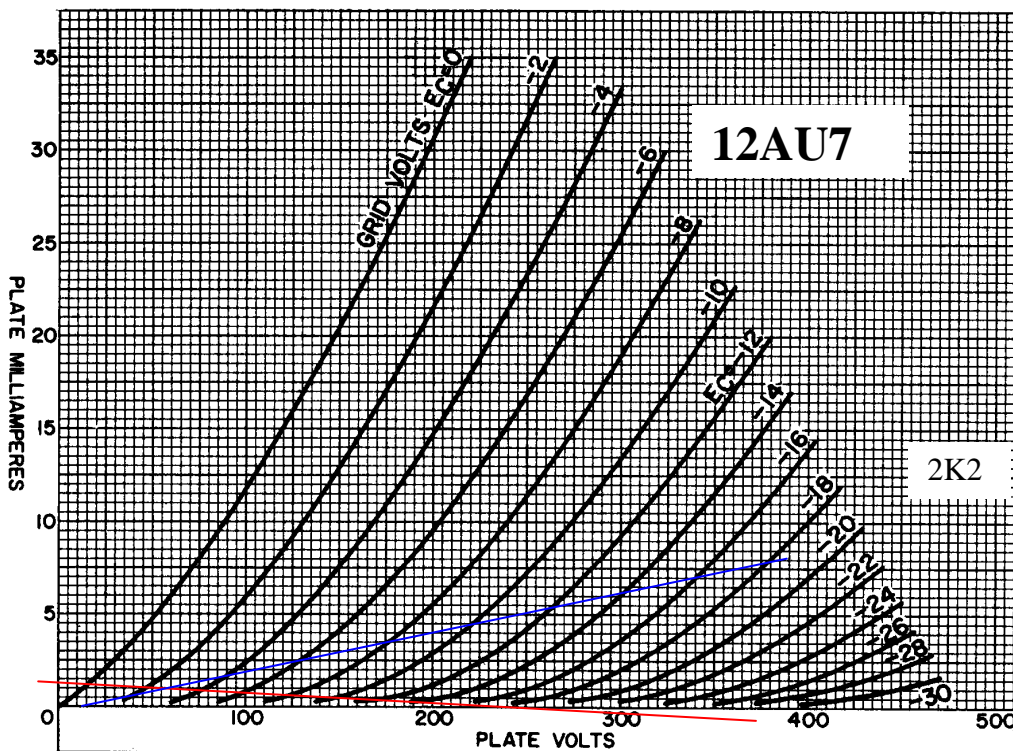


3.3 Phase Inverter stage – 12AX7 in split-load (cathodyne) config

VS3= 250V. Rk=2k2. Vgk=1.3V. Vk=61.3V. Va=192V. Vak= 130V. Anode current = (250-192)/100k=0.6mA.



Changing to a 12AU7 will draw more current, and raise the cathode bias to ? The anode/cathode loads should be reduced from 100k to about 47k, and the supply dropper reduced from 27k to 15k



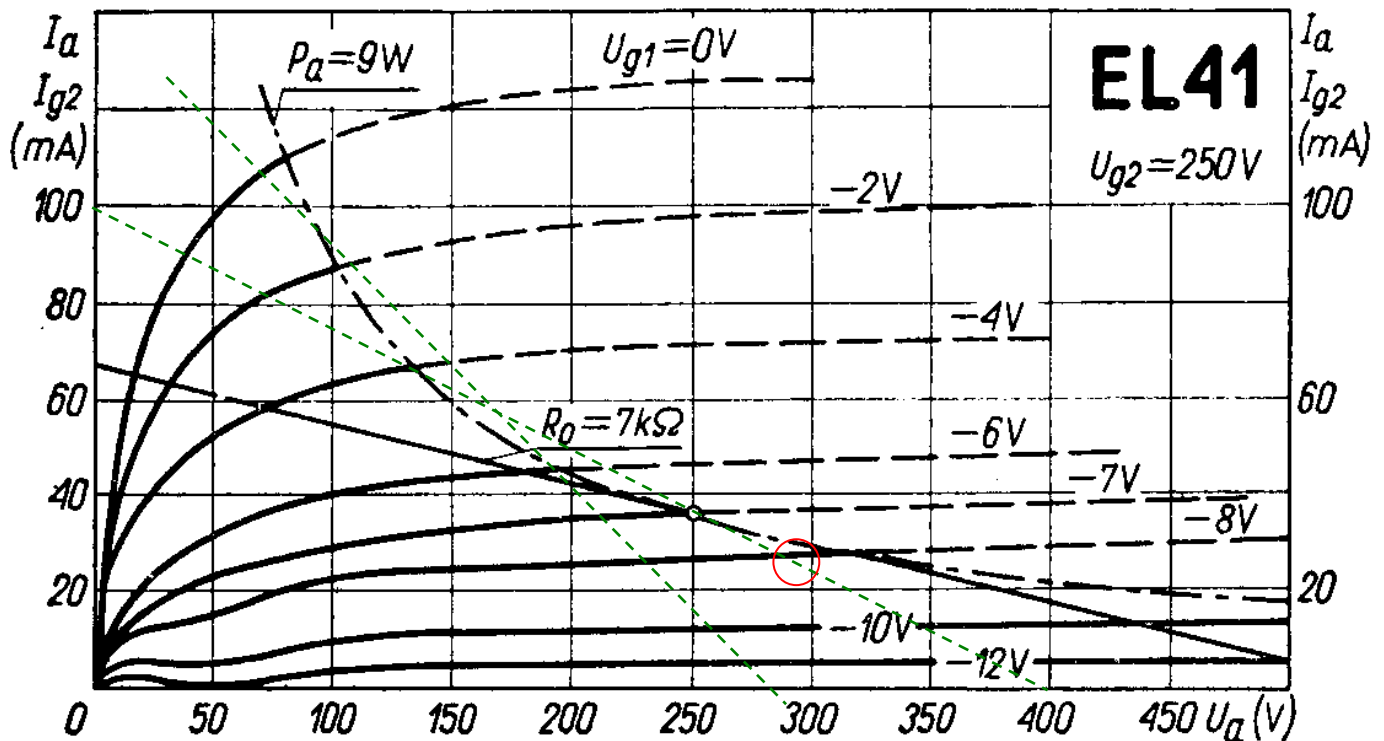
3.4 Output Stage

Class AB push-pull output stage, common cathode bias. The 8KΩ impedance plate-to-plate OPT presents signal currents into each tube with a 4KΩ impedance with both tubes conducting, to 2KΩ load impedance at higher levels. No pentode characteristic curves are available for 6M5, and similar EL41 curves are shown but at a lower 250V screen (actual screen is about 280V at idle so bias voltage is close to 10V).

As the output loading increases, the supply voltage VS1 to the output valve plates sags from about 300-10=290V towards 290V. Plate DC voltage will be lower than VS1 by an amount up to ~28V (ie. plate-cathode sags to about 260V) due to OPT half resistance of about 95Ω with a peak current of up to about 0.1A, and cathode bias drop of 18V. Screen voltage will vary from about 280 towards 265V under steady-state heavy load (ie. screen-cathode sags to about 265-18 = 245V).

The maximum output valve bias current allowed is dependant on the maximum recommended plate dissipation – assume 75% of 9W = 6.8W: $I_{bias(max)} = P_d / V_b = 6.8W / 290V = 23mA$, or about 25mA of cathode current.

For a peak plate current of 100mA, then the nominal output power of the amplifier would be: $(I_{pk})^2 \times R_{pp} / 8 = 0.1 \times 0.1 \times 8k / 8 = 10W$. For this maximum signal condition, the rms OPT current draw is likely about 64mA (64% of peak), and the average VS1 power consumed is about 260V x 0.064Arms = 17W, and the OPT loss is about $(0.064)^2 \times 190\Omega = 0.8W$, so the tube plates dissipate $17 - 9.4W - 0.8W = 7W$, or just under 3.5W each, which is well below max design level.



3.5 Power Supplies

The 6V4 is rated to feed 50uF with secondary winding resistance $>125\Omega$ from 250VAC, and 90mA loading for a 265VDC output, and has a hot switch peak current rating of 900mA, and a continuous peak current rating of 270mA.

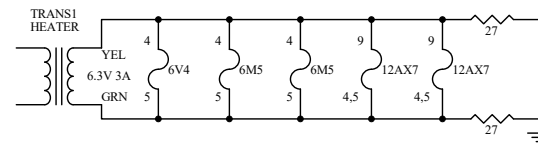
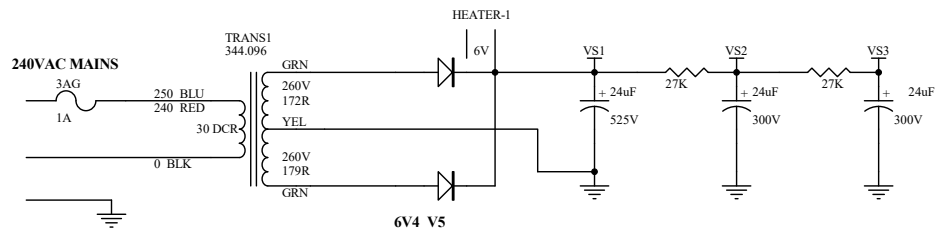
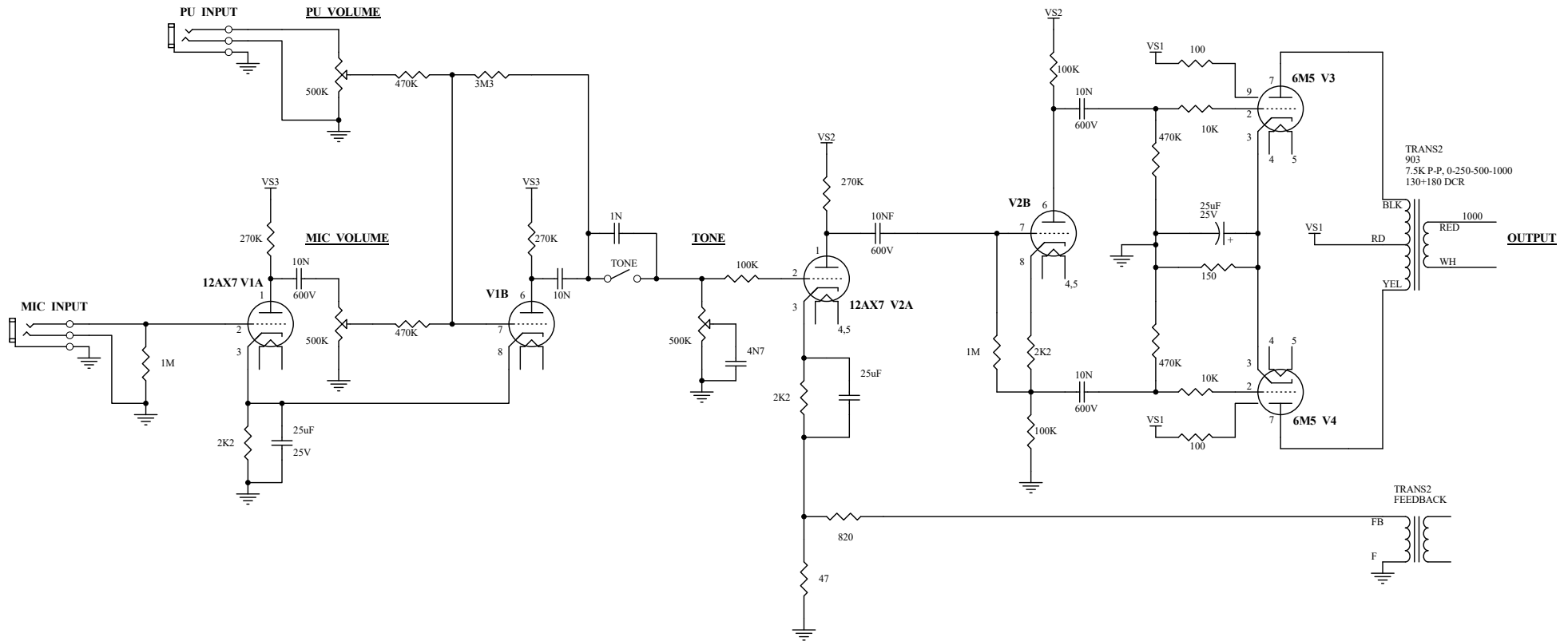
The effective series resistance is $30\Omega \times (260/250)^2 + 185\Omega = 220\Omega$, which is fine.

PSUD2 indicates a hot switched peak of up to 900mA, and a steady-state continuous of 240mA_{pk} at idle, which appears to be fine for cranked output. The steady-state PT secondary CT current at idle is about 110mA_{rms}, and rising to 570mA_{rms} for a 10ms period for a hot switch event, which would allow a 200mA Fast IEC127 fuse to be used (min rating of 50ms at 2.75x rating multiplier).

A 1.6H @ 60mA_{dc}, DCR=430 Ω (Wurlitzer 500409) choke is added in series with 1k dropper from VS1 to VS2 to reduce screen voltage ripple from 1.6V_{rms} to 0.3V_{rms}.

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Original

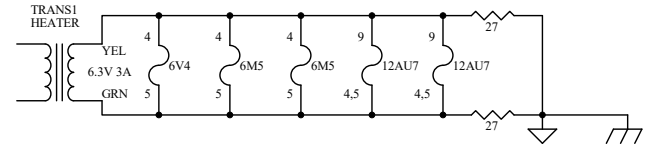
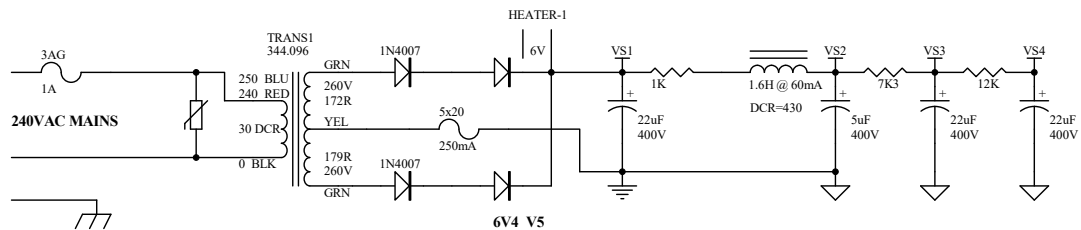
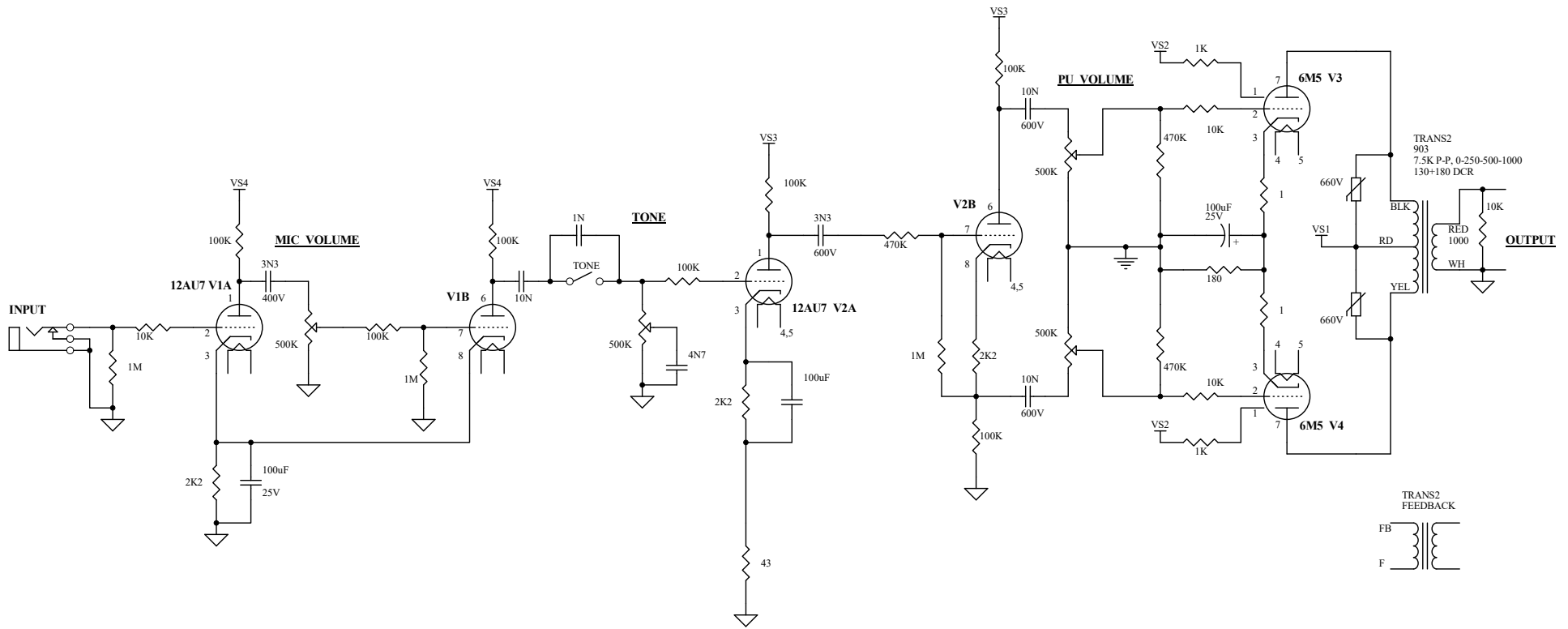


VOLTAGE RAIL	IDLE	VALVE	QTY
VS1	285V	6M5	2
VS2	250V	6V4	1
VS3	216V	12AX7	2
HEATER-1	6.3V		

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Modified



VOLTAGE RAILS		VALVE QTY	
RAIL	IDLE	6M5	12AU7
VS1	300V, 5.4Vrms	2	1
VS2	280V, 0.3Vrms	1	2
VS3	250V		
VS4	225V		
HEATER-1	6.5V		

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